

Neural Network Contour Error Prediction of a Bi-Axial Linear Motor Positioning System

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Abstract: In the article a method of predicting contour error using artificial neural network for a bi-axial positioning system is presented. The machine consists of two linear stages with permanent magnet linear motors controlled by servo drives. The drives are controlled from a PC with real-time operating system via EtherCAT fieldbus. A randomly generated Non-Uniform Rational B-Spline (NURBS) trajectory is used to train offline a NARX-type artificial neural network for each axis. These networks allow prediction of following errors and contour errors of the motion trajectory. Experimental results are presented that validate the viability of the neural network based contour error prediction. The presented contour error predictor will be used in predictive control and velocity optimization algorithms of linear motor based CNC machines.

1 INTRODUCTION

Multi axis machines are widely used in industrial manufacturing in the form of numerically controlled machine tools (CNC) and robots. Each mechanical axis is driven by a linear or rotary feed drive. Composition of their movements constitutes the output motion trajectory of the machine's end effector (i.e. milling tool, laser head, welding head, gripper) also called a toolpath. Position commands for each feed drive are generated by interpolating the given tool path according to pre-planned or on-line generated velocity profiles.

In order to enhance machine performance much attention has been given to improving the motion planning process by developing new feedrate profile generation algorithms. Several authors propose using optimization algorithms to generate an optimal feedrate profile (Xu et al., 2018; Ni et al., 2018; Zhang et al., 2019). An optimal feedrate profile maximizes speed while simultaneously respecting the feed drives' and machine's constraints in order to shorten machining time. Most approaches neglect the influence of machining errors in the feedrate planning process. Machining errors are often defined as contour

errors which are the minimum distances between the reference toolpath and actual tool positions (Ramesh et al., 2005; Tang and Landers, 2013) as shown in figure 1. Some authors propose including error constraints in the feedrate planning process but usually use simplified models that do not accurately predict actual following errors (Jia et al., 2017).

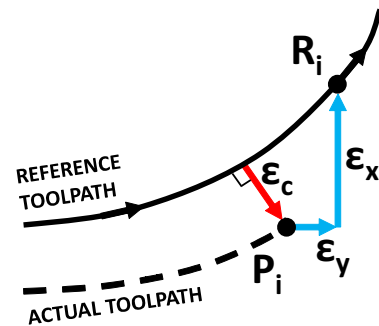




Figure 1: Contour error definition. ϵ_c - contour error, $\epsilon_{x,y}$ - axis following errors, R_i - toolpath reference point, P_i - actual toolpath point.

Optimizing feedrate with respect to contour error constraints is especially important for machines that utilize linear motor feed drives such as laser cutters. These machines can achieve very high speeds and accelerations which significantly reduces machining time. At the same time they simultaneously

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need to ensure accurate toolpath following. Most multi axis machines use permanent magnet rotary synchronous motors which produce rotary motion and torque. Some mechanism is usually required to convert rotation into linear motion. These are usually ballscrews, racks and pinions or toothed belts sometimes with an additional reduction gear. Permanent magnet linear synchronous motors produce linear motion directly without the need for additional mechanisms. This has the advantage of greatly simplifying the machines construction and eliminating backlash and compliance in the feed drive which leads to decreased following errors. On the other hand the linear motor does not have the mechanical advantage provided by these mechanisms and has to drive the machines mass directly. Linear motors are controlled using the same field oriented control techniques used in rotary motors therefore the same servo drives can usually be used.

The authors previously developed a feedrate optimization method which accounts for contour error for traditional ballscrew driven machines (Erwinski et al., 2016; Szczepanski et al., 2017). A fundamental requirement for such an algorithm is an accurate model of the entire feed drive (both the servo drive and the mechanical part). This model is used during optimization to constrain the maximum contour error by adjusting the feedrate profile. There is currently ongoing work by the authors to extend and improve this approach on linear motor based machines which offer significantly higher speeds and accelerations. It is important that the model used is easy to identify and can be easily ported to any machine with any servo drive. To this end a black-box neural-network based contour error predictor is proposed that accounts for the dynamics of both the servo drive and mechanical components of the linear motor feed drive.

2 BI-AXIAL LINEAR MOTOR POSITIONING SYSTEM

The linear motor positioning system used in this research consists of two linear motor positioning units representing X and Y axes of a multi-axis machine. The positioning units use Tecnotion TM6 iron core flat linear motors mounted on an aluminium chassis with linear roller guideways. The motors are controlled by Kollmorgen AKD-P00307 servo drives with feedback provided by Renishaw optical linear scales. The high resolution feedback provides positioning accuracy of around 0.01 micrometre. The positioning units' servo drives receive position, velocity or torque commands from a PC-based numeri-

cal controller via EtherCAT fieldbus (Jansen and Butner, 2004; Paprocki et al., 2018). The PC controller runs TwinCAT 3 real-time control software on a standard Windows 10 operating system. Special real-time mechanism implemented in TwinCAT such as processor core isolation ensure hard real-time operation of the CNC controller. This allows for implementation of typical PLC or CNC controllers in software without any dedicated hardware extensions. TwinCAT also implements a real-time EtherCAT communication stack and driver which enables deterministic communication with many commercial automation equipment such as servo drives or input output devices.

TwinCAT also enables the user to implement custom real-time control programs in C++. This approach was used in this research to develop a trajectory interpolator for both linear axes. The interpolator generates position commands in 250 microsecond intervals and sends them over EtherCAT to the drives to realize the reference motion trajectory. The developed software can also send direct commands to the drive over Ethercat to initiate the device, perform homing, clear errors and change between position, velocity and torque modes according to the Can in Automation CIA402 device profile. The picture of the linear motor positioning system test stand is shown of figure 2 and its schematic is shown of figure 3.

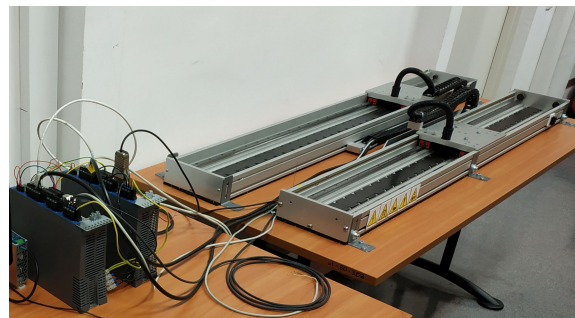


Figure 2: Linear motor positioning system test stand

The linear motor motion path is defined as a third order Non-Uniform Rational B-Spline (NURBS) (Piegl and Tiller, 2012). Such path description is often used in CNC machining because of guaranteed continuity, ability of local shape modification and ability to easily describe complex shapes (Heng and Erkorkmaz, 2010; Liu et al., 2015). Interpolation of NURBS toolpaths is performed according to a predefined, optimized polynomial feedrate profile. This allows to maximize drive capabilities without violating their speed and acceleration limits.

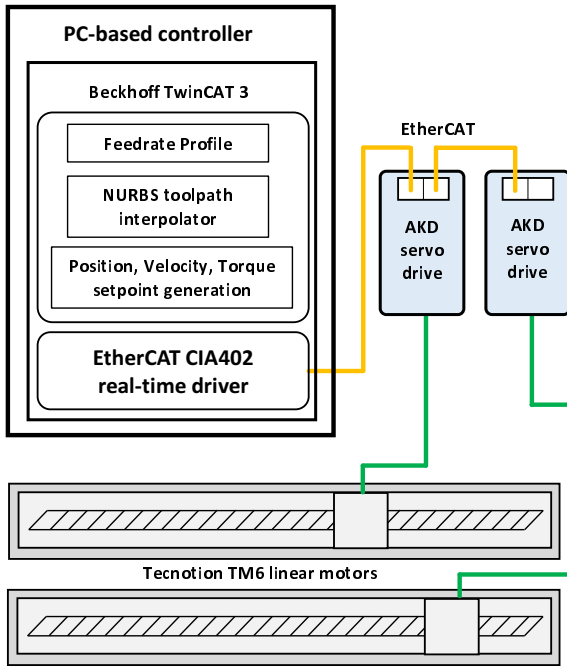


Figure 3: Linear motor positioning system test stand schematic

3 LINEAR MOTOR FEED DRIVE MODEL

Main factors that contribute to the dynamics of the linear motor positioning system are the mass of the motor and carriage attached to it and guideway friction. Due to lack of drive train effects such as backlash or compliance do not influence the positioning accuracy. An additional effect typical of flat iron core linear motors is the cogging force. This force is due to the attraction between the motor's iron core and the permanent magnets and is dependent on their relative position. This causes a periodic force ripple the frequency of which is proportional to the motor speed and magnet pitch (distance between adjacent magnet poles). The cogging force has significant effect on positioning accuracy mainly at low speeds. Because this effect depends only on motor position it can be mapped and eliminated by using static feedforward compensation. This functionality is implemented in the Kollmorgen AKD servodrives and was used in this research to significantly eliminate its effect on positioning accuracy.

Friction force is influenced by several friction components. When the drive tries to move the motor from standstill it has to overcome static friction. Then as the speed increases the friction force drops and after reaching a certain speed rises again. This is called the Stribeck effect and the velocity at which

the friction minimum is reached is the Stribeck velocity. Friction then increases as a linear function of speed and this component is called the viscous friction. There is also a constant velocity independent component called the Coulomb friction which depends only on mass. Friction is usually assumed to be symmetric for positive and negative velocities. This is not always the case if the motion unit is inclined or the guideways are not exactly parallel to each other. A block schematic of the linear motor feed drive is presented in figure 4.

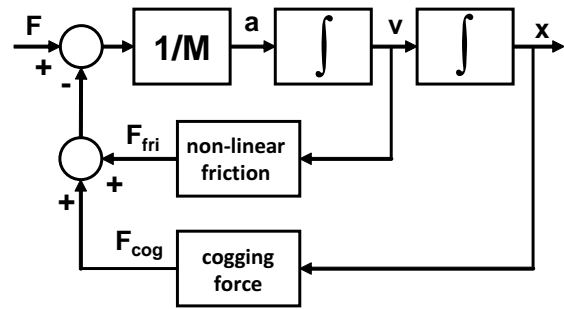


Figure 4: Linear motor model, M - motor and carriage mass, a - motor acceleration, v - motor speed, x - motor position, F_{fri} - friction force, F_{cog} - cogging force.

In order to identify the Linear Motor Feed Drive Model a series of experiments were performed on the system. In order to identify carriage mass a current step command of 2A was issued and actual velocity was measured. Total carriage and motor force mass was identified using MATLAB System Identification Toolbox to be 3.61kg. In order to identify friction a series of constant positive and negative velocity movements were performed in velocity mode from 0.1 mm/s to 2000 mm/s. Motor current was measured for each run in order to determine the friction force. This current was averaged to eliminate any force ripples and multiplied by the motor force factor K_f . The resulting friction map is shown in figure 5.

It can be clearly seen that for large velocities from about 500mm/s the viscous does not increase linearly with the increase in speed as is usually assumed. The discrepancy between a linear friction characteristics and actual friction curve is significant at large speeds. For 2 m/s the actual friction current is 20% smaller than a linear friction model would predict. The linear motor also has a large static friction requiring about 500mA current to start movement. This was identified by generating a ramp current command and recording the amount of current at which the motor starts to move. This is caused by large magnet attraction forces and lack of mechanical advantage offered by traditional drive train mechanisms.

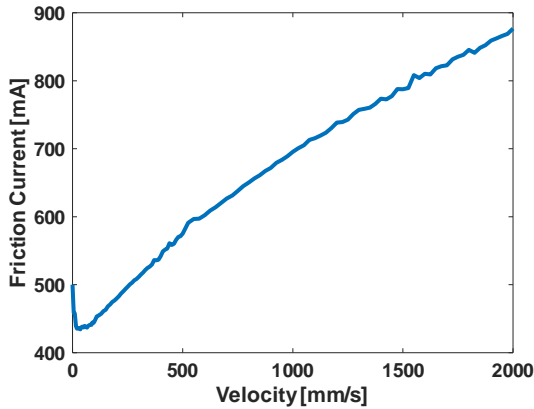


Figure 5: Current due to friction as a function of velocity.

It is clear that the linear motor positioning system although mechanically very simple has non-linear characteristics. Identification of a model presented in fig. 4 is time consuming and requires switching the drive to velocity and torque modes. This is not always possible on commercial multi-axis machines. Also when using off-the-shelf servo drives the actual controller structure is not always precisely known. Due to these problems a black box modelling approach is used instead in order to obtain following and contour error predictions.

4 NARX NEURAL NETWORK CONTOUR ERROR PREDICTION

In order to obtain contour error predictions of a linear motor positioning system with NURBS motion path definition following error prediction of each axis have to be determined first. Predicted following errors are combined with information about local toolpath geometry to obtain and estimated contour error. The structure of a neural network contour error predictor is shown in figure 6.

Prediction of axis following errors is performed by using a Non-Linear Auto Regressive Exogenous Input Neural Network (NARX). Such networks differ from traditional multi-layered perceptrons (MLP) by adding a feedback between output and input layers and delays in the input layer. This allows to model non-linear dynamical systems. An example of a NARX neural network used for following error prediction is presented in figure 7. Reference velocity obtained from differentiating polynomial toolpath and feedrate profile is used as input.

Training the network is a process of minimizing

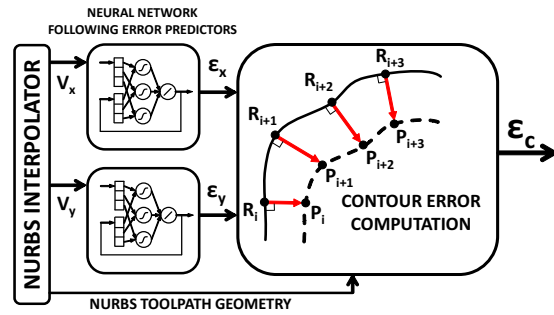


Figure 6: Structure of neural network prediction block

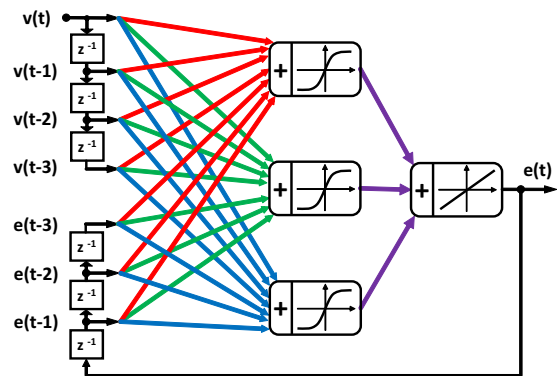


Figure 7: Example structure of a NARX neural network used for following error prediction

the mean squared errors based on error backpropagation. Training of the NARX following error predictor is performed first in series-parallel form where the network feedback is disconnected and target series (following error) is fed into the network along the input signal (reference velocity). In this form standard static network training algorithms are used (Xie et al., 2009). Training is finished when the prediction error stops decreasing. The feedback is then reconnected and training is continued in parallel form. In this form dynamic training algorithms such as backpropagation through time have to be used. These are more computationally demanding and are sensitive to initial weight values (Horne and Giles, 1995). Weights obtained from the series-parallel training phase are used as initial guess for parallel training which gives good initial values and decreases total training time. Training is finished when the prediction error does not change significantly for some period of time. MATLAB Neural Network Toolbox function TRAINBR is used to train the network.

If motion paths are defined as Non-Uniform Rational B-Splines (NURBS) or other polynomial curves the contour error cannot be computed exactly and has to be estimated (Uchiyama et al., 2011). Several contour error estimation techniques for free-form

toolpaths have been proposed (Yeh and Hsu, 2002; Huo et al., 2012; Sencer et al., 2009; Chen et al., 2008). All of these are either simple estimates which have large errors for curves with high curvatures or are computationally demanding. In one interesting algorithm proposed in (Zhu et al., 2013) the contour error vector is approximated by a Taylor series which yields accurate estimates without high computational demand. This method was chosen for developing the contour error predictor. The contour error is estimated using the following closed form formula:

$$\vec{\epsilon}_c = \left[-\vec{c} - \frac{1}{2} \frac{\kappa(\hat{c} \cdot \hat{n})(\hat{t} \cdot \vec{\epsilon}_t)\hat{t}}{1 - \kappa(\hat{c} \cdot \hat{n})} \right] \cdot \vec{\epsilon}_t \quad (1)$$

$$\hat{c} = -\frac{\vec{\epsilon}_t \cdot \hat{t}}{\sqrt{\|\vec{\epsilon}_t\|^2 - \vec{\epsilon}_t \cdot \hat{t}}} \hat{t} + \frac{1}{\sqrt{\|\vec{\epsilon}_t\|^2 - \vec{\epsilon}_t \cdot \hat{t}}} \vec{\epsilon}_t \quad (2)$$

where: κ - toolpath curvature at the reference point, \hat{t}, \hat{n} - tangent and normal unit vectors at the reference point, $\vec{\epsilon}_t$ - following error vector. Curvature, tangent and normal vectors can be computed using the following formulas:

$$\kappa = \frac{\|C'(u) \times C''(u)\|}{\|C'(u)\|^3} \quad (3)$$

$$\begin{aligned} \hat{t} &= \frac{C'(u)}{\|C'(u)\|} \\ \hat{b} &= \frac{C'(u) \times C''(u)}{\|C'(u) \times C''(u)\|} \\ \hat{n} &= \frac{\hat{b}(u) \times C'(u)}{\|\hat{b}(u) \times C'(u)\|} \end{aligned} \quad (4)$$

where: $C'(u), C''(u)$ - are first and second derivatives of the NURBS toolpath position vector with respect to the toolpath parameter u obtained from the NURBS interpolator.

5 EXPERIMENTAL RESULTS

In order to generate training data for the contour error predictor a NURBS trajectory was constructed by randomly generating curve control points in the whole positioning system travel range between 0 and 1200mm in both axes. The toolpath used is presented in figure.

A feedrate profile was generated which forced high variations and values of velocity, acceleration and jerk in each axis while simultaneously keeping them within safe limits. The maximum values of velocity, acceleration and jerk were $2500mm/s$, $25000mm/s^2$

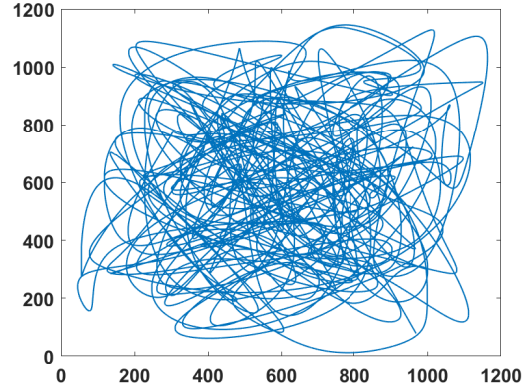


Figure 8: Butterfly NURBS curve motion path.

and $500000mm/s^3$ respectively. This was done to sufficiently capture following error dynamics and avoid drive saturation and positioning system damage. The feedrate profile and motion path were run using the PC-based controller controlling the linear motor positioning system. Axis velocity demand and actual contour error was recorded and transferred to MATLAB. A NARX neural network with 5 input, 4 feedback delays and 6 sigmoid hidden neurons was used to train following error predictor for X and Y axes. The size of the network was chosen by the authors by performing multiple training sessions of multiple networks of different size and choosing the one which achieved best performance (lowest error). The obtained neural network contour error predictor was used to verify contour error prediction accuracy of a butterfly curve (figure 9). The curve was run on the linear motor positioning system and actual contour error was computed and compared with values predicted from the proposed predictor.

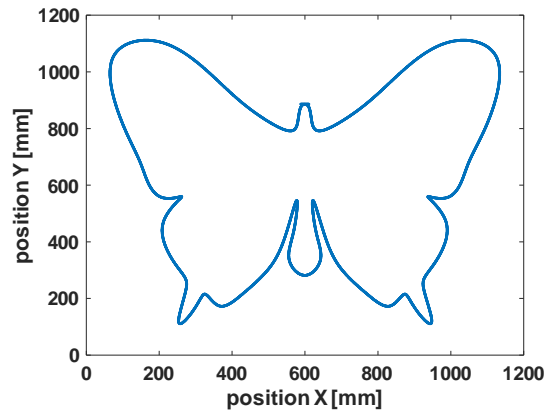


Figure 9: Butterfly NURBS curve motion path.

Figure 10 presents a comparison of following and

contour error resulting from realizing the actual motion path and predicted using the NARX contour error predictor. The mean squared error (MSE) of contour error prediction is $2.6921e-04$ mm. It can be seen that the predictor is able to accurately predict actual following errors and by extent the actual contour error. It should be noted that the test toolpath was not used in the neural network training process and the accurate prediction is due to neural network generalization abilities.

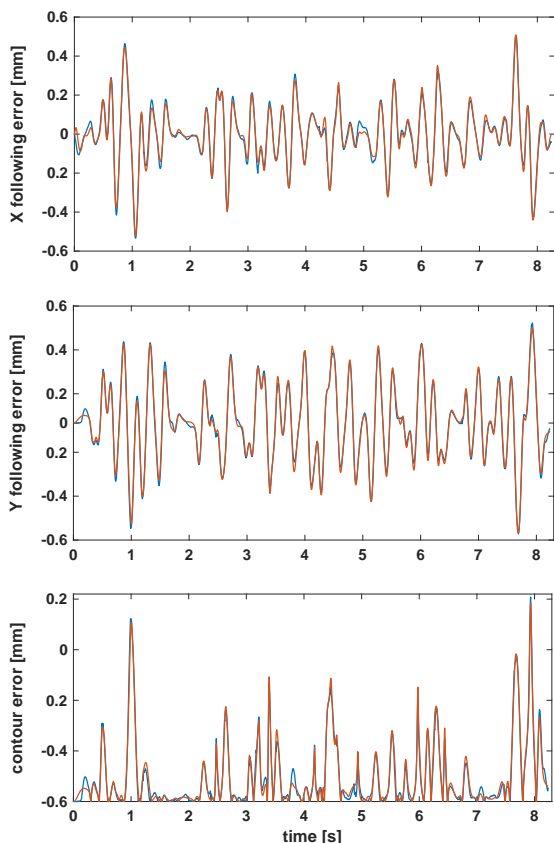


Figure 10: Predicted (orange) and actual (blue) following error and contour error for validation dataset (butterfly curve).

6 CONCLUSION

The article presents a contour error predictor for a bi-axial linear motor positioning system based on neural networks. It is shown that a linear motor exhibits non-linear dynamics mainly due to non-linear friction at very low and very high speeds. Due to complexity of identifying particular friction components and potentially incomplete information about

the commercial drive control structure a black box approach to predicting contour error is proposed. This approach uses NARX neural networks to predict following errors of each axis. This in turn is used to estimate contour error based on local motion path geometry.

Experimental results show good accuracy in predicting contour error of a NURBS motion path. Major advantage of this approach is the quick and easy identification procedure. Actual toolpaths can be used with following errors obtained during normal machine operation. Identification experiments in velocity and torque modes are not required. The neural network can generalize and accurately predict actual following and contour errors for toolpaths not used in the training process.

The main contribution of this paper is developing a fast and easy to use method to predict contouring error in multi axis positioning systems such as CNC machine tools. The contour error predictor will be used to develop an on-line feedrate optimization method for linear motor based multi axis machines. It can also be used for predictive control of such machines.

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